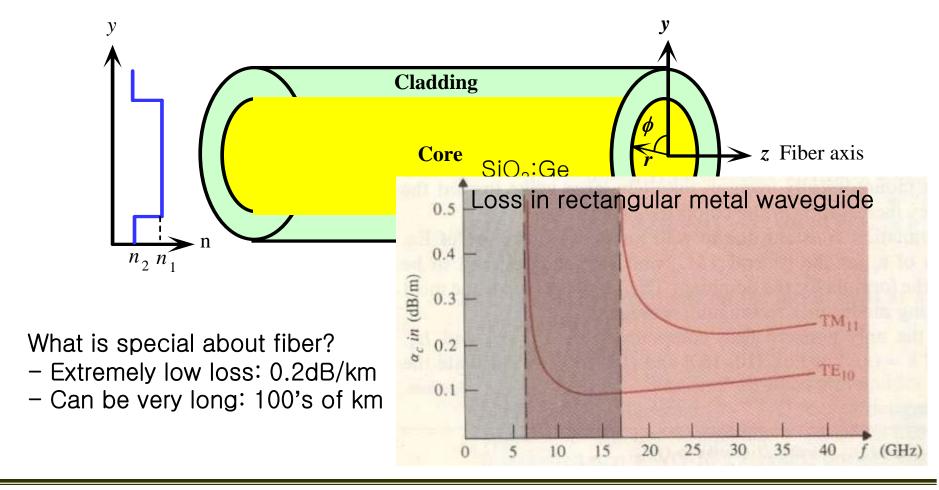
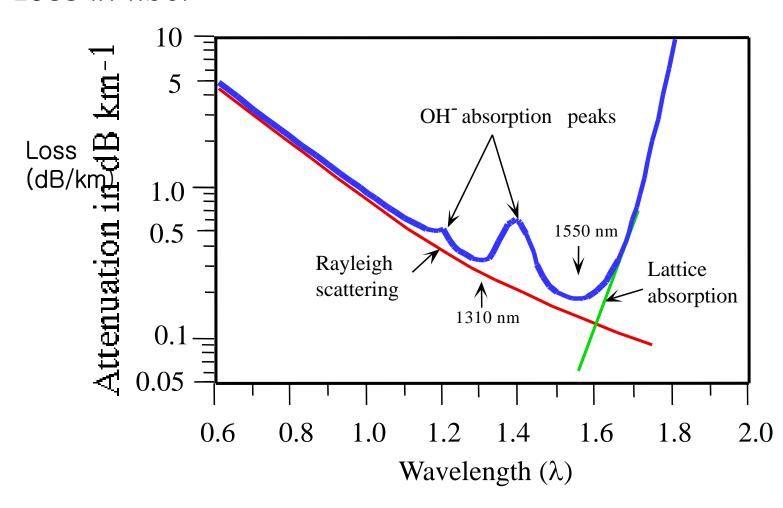
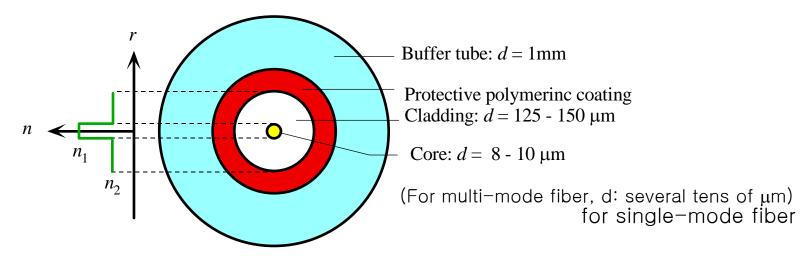
Optical Fiber: Circular dielectric waveguide made of silica (SiO₂)



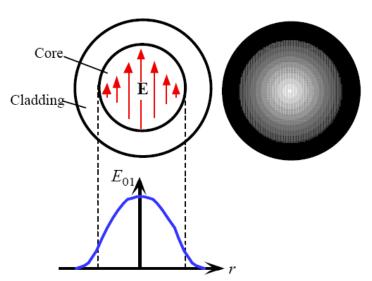
Loss in fiber

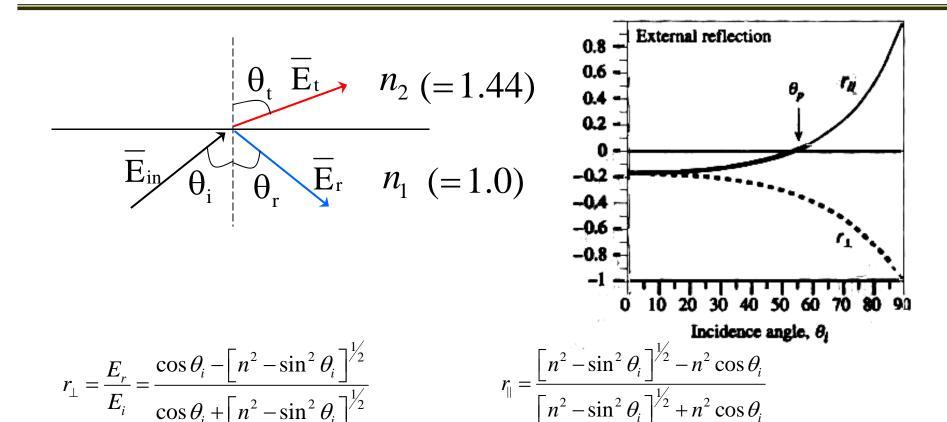




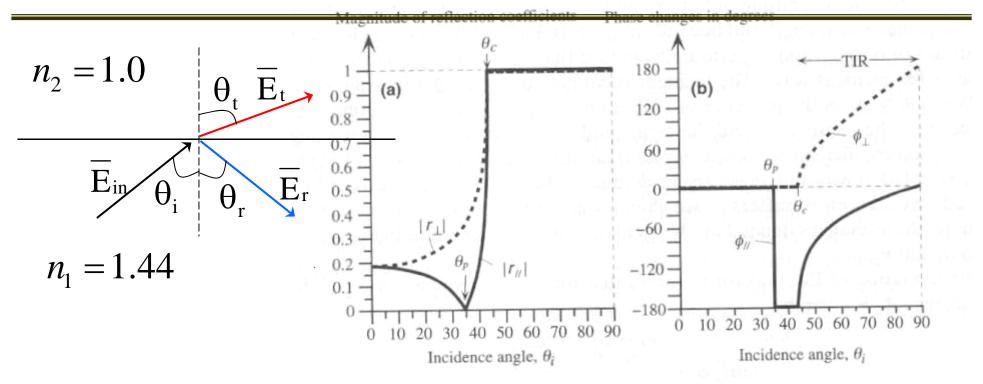
Optical Power Distribution In Single-Mode Fiber

What confines light inside core?





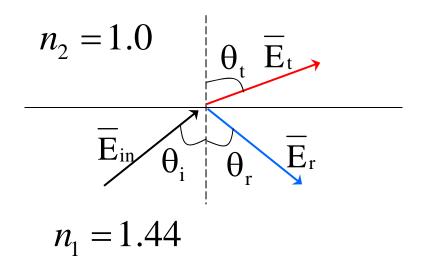
$$t_{\perp} = \frac{E_t}{E_i} = \frac{2\cos\theta_i}{\cos\theta_i + \left\lceil n^2 - \sin^2\theta_i \right\rceil^{1/2}} \quad (n = \frac{n_2}{n_1}) \qquad t_{\parallel} = \frac{2n\cos\theta_i}{\left\lceil n^2 - \sin^2\theta_i \right\rceil^{1/2} + n^2\cos\theta_i}$$

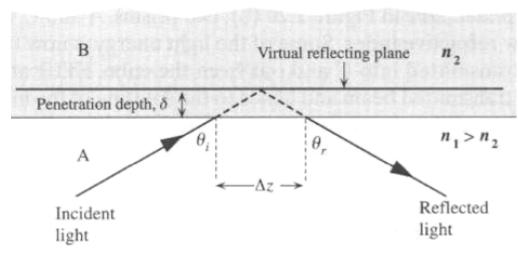


What happens at $\theta_c = \sin^{-1} n$?

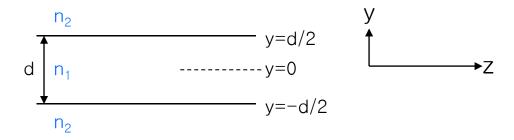
$$r_{\perp} = \frac{E_r}{E_i} = \frac{\cos \theta_i - \left[n^2 - \sin^2 \theta_i \right]^{\frac{1}{2}}}{\cos \theta_i + \left[n^2 - \sin^2 \theta_i \right]^{\frac{1}{2}}}$$

r becomes complex!(magnitude 1, phase shift)





3-layer dielectric waveguide

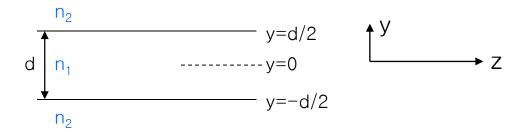


Full analysis starting from wave equations.

$$\nabla^{2}\overline{E}(y,z,t) = \mu\varepsilon \frac{\partial^{2}\overline{E}}{\partial t^{2}}(y,z,t)$$
Assuming $\overline{E}(y,z,t) = \overline{E}(y,z) \cdot e^{j\omega t}$,
$$\nabla^{2}\overline{E} + k^{2}(y)\overline{E} = 0, \text{ where } k^{2}(y) = \mu\varepsilon(y)\omega^{2}$$

$$k(y) = n_{2}k_{0} \text{ for } |y| > \frac{d}{2}; \text{ cladding}$$

$$k(y) = n_{1}k_{0} \text{ for } |y| < \frac{d}{2}; \text{ core}$$



Consider TE Solution.

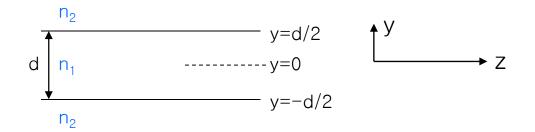
$$\overline{E}(y,z) = \overline{x} E(y) e^{-j\beta z}$$

Then,
$$\frac{d^2 E(y)}{dy^2} + (k^2(y) - \beta^2)E(y) = 0$$

=> Eigen value equation. Solve for β and E(y)

$$k^{2}(y) - \beta^{2} > 0$$
 in core $=> E(y) \sim \sin(k_{y}y)$ or $\cos(k_{y}y)$ with $k_{y} = \sqrt{(n_{1}k_{0})^{2} - \beta^{2}}$

$$k^2(y) - \beta^2 < 0$$
 in cladding $\Rightarrow E(y) \sim \exp(\alpha y)$ or $\exp(-\alpha y)$ with $\alpha = \sqrt{\beta^2 - (n_2 k_0)^2}$



Solutions

$$y > \frac{d}{2} : E(y) = A \exp(\alpha y) + B \exp(-\alpha y)$$

$$|y| < \frac{d}{2} : E(y) = C \sin(k_y y) + D \cos(k_y y)$$

$$y < -\frac{d}{2} : E(y) = E \exp(\alpha y) + F \exp(-\alpha y)$$

Here, A=0 and F=0.

For easy analysis, divide the solutions into even and odd solutions



Even Solutions

$$y > \frac{d}{2} : E(y) = B \exp(-\alpha y)$$

$$|y| < \frac{d}{2} : E(y) = D \cos(k_y y)$$

$$y < -\frac{d}{2} : E(y) = B \exp(\alpha y)$$

$$(E = B)$$

Apply boundary conditions:

$$E(y) \text{ and } \frac{dE(y)}{dy} \text{ are continuous at } y = \pm \frac{d}{2}$$

$$B \exp(-\alpha \frac{d}{2}) = D \cos(k_y \frac{d}{2}) \qquad ----- (1)$$

$$-\alpha B \exp(-\alpha \frac{d}{2}) = -k_y D \sin(k_y \frac{d}{2}) ----- (2)$$

$$\frac{(2)}{(1)} = > \alpha = k_y \tan(k_y \frac{d}{2})$$

Odd Solutions

$$y > \frac{d}{2} : E(y) = B \exp(-\alpha y)$$

$$|y| < \frac{d}{2} : E(y) = D \sin(k_y y)$$

$$y < -\frac{d}{2} : E(y) = -B \exp(\alpha y)$$

$$(E = -B)$$

Apply boundary conditions.

$$E(y) \text{ and } \frac{dE(y)}{dy} \text{ are continuous at } y = \pm \frac{d}{2}$$

$$B \exp(-\alpha \frac{d}{2}) = D \sin(k_y \frac{d}{2}) \quad ----- (1)$$

$$-\alpha B \exp(-\alpha \frac{d}{2}) = k_y D \cos(k_y \frac{d}{2}) \quad ----- (2)$$

$$\frac{(2)}{(1)} \Longrightarrow \alpha = -k_y \cot(k_y \frac{d}{2}) = k_y \tan(k_y \frac{d}{2} - \frac{\pi}{2})$$

y=-d/2 Even: $\alpha = k_y \tan(k_y \frac{d}{2})$

What do these mean?

Odd:
$$\alpha = k_y \tan(k_y \frac{d}{2} - \frac{\pi}{2})$$

Determine k_y and α that satisfy above conditions.

For graphical analysis, do following normalization.

Let
$$X = k_y \frac{d}{2}$$
, $Y = \alpha \frac{d}{2}$

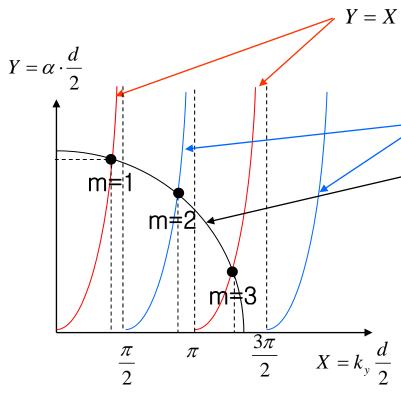
Then, $Y = X \tan X$ for even

$$Y = X \tan(X - \frac{\pi}{2})$$
 for odd

Plot these on X-Y plane.

But
$$X^2 + Y^2 = \left(\frac{d}{2}\right)^2 (k_y^2 + \alpha^2) = \left(\frac{d}{2}\right)^2 [(n_1 k_0)^2 - \beta^2 + \beta^2 - (n_2 k_0)^2]$$

= $\left(\frac{d}{2}\right)^2 k_0^2 (n_1^2 - n_2^2) = r^2$



 $Y = X \tan X$: even mode

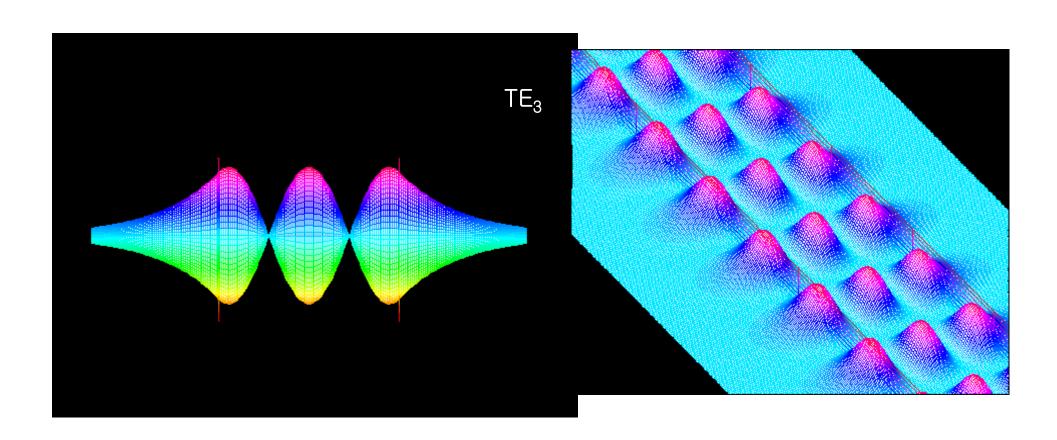
 $Y = X \tan(X - \pi/2)$: odd mode

$$X^{2} + Y^{2} = \left(\frac{d}{2}\right)^{2} k_{0}^{2} (n_{1}^{2} - n_{2}^{2}) = r^{2}$$

Observations:

- Points where circle and tangent curves intersect are solution points for k_y and α (TE mode).
 With larger r (larger d, smaller λ, larger
 - With larger r (larger d, smaller λ , larger $n_1^2 n_2^2$), more modes exist.
 - There is at least one even mode.
 - Even, odd, even, odd ...

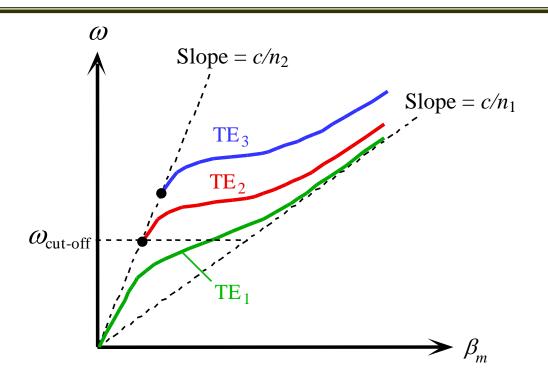
E(y) profile: $n_1=1.5$, $n_2=1.495$, $d=10\mu m$, $\lambda=1\mu m$



Wave is not entirely confined within core: Confinement factor

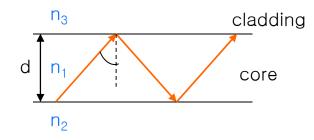
not entirely confined within core: Confin
$$\Gamma = \frac{\text{Power inside core}}{\text{Total Power}} = \frac{\int_{y=-\frac{d}{2}}^{y=\frac{d}{2}} |E(y)|^2 dy}{\int_{y=-\infty}^{y=-\frac{d}{2}} |E(y)|^2 dy}$$

For higher modes, how does Γ change?



Group velocities are different for different modes => modal dispersion Need a single-mode waveguide in order to avoid signal distortion. How do you design a single mode waveguide?





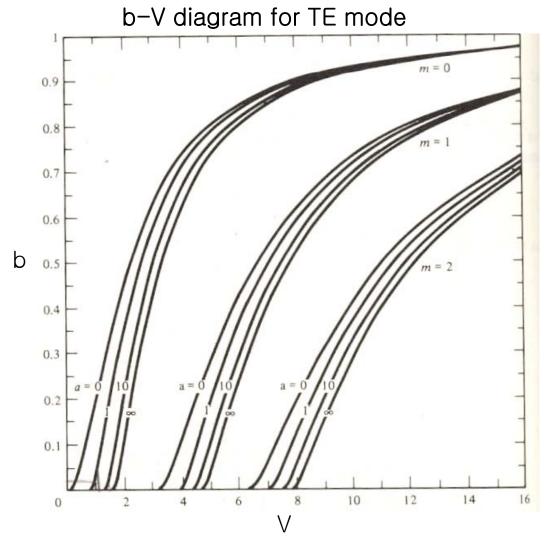
$$V = k_0 d(n_1^2 - n_2^2)^{\frac{1}{2}}$$
(Normalized k)

$$b = \frac{\left(\frac{\beta}{k_0}\right)^2 - n_2^2}{n_1^2 - n_2^2}$$

(Normalized β)

$$a = \frac{n_2^2 - n_3^2}{n_1^2 - n_2^2}$$

(Asymmetry factor)



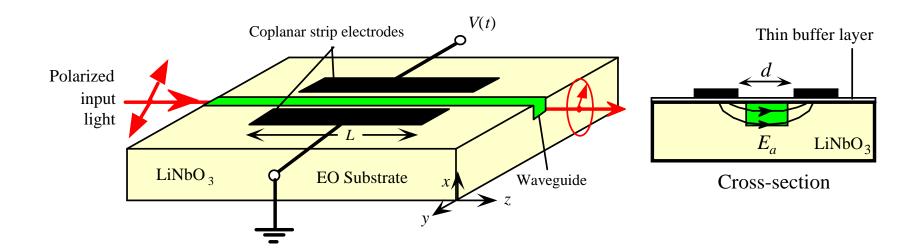
Issues for practical waveguides

- Precise control of dimension and refractive index
- Low loss at desired λ
- Mass production possible
- Integration desirable (Integrated Optics)
- Electrical control of refractive index (Electro-Optic effect)

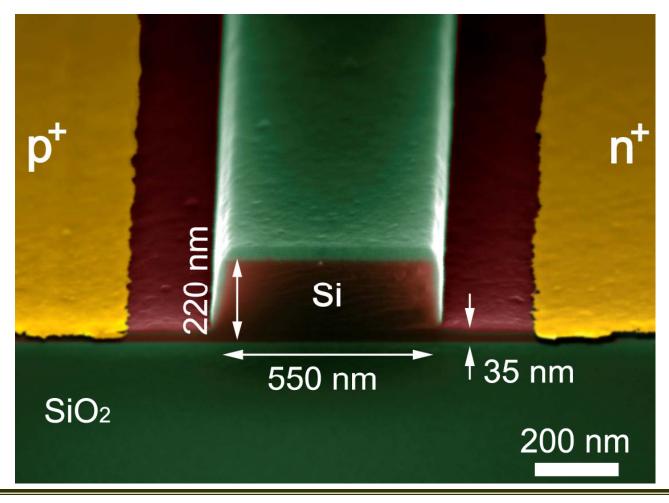
Materials used for waveguides

- Silica → Optical fiber
- Semiconductors: GaAlAs, InGaAsP, Si/SiO₂
- Dielectric materials: LiNbO₃ with Ti doping

LiNbO₃ waveguide



Si/SiO waveguide



Problem 1

Several different types of waveguides having the same core material and thickness are shown below.

$$y = d$$

$$y = 0$$

$$m_{2} = 1$$

$$m_{2} = 1$$

$$m_{2} = 1$$

$$m_{2} = 1.5$$

$$m_{2} = 1$$

$$m_{2} = 2$$

$$m_{2} = 2$$

$$m_{2} = 2$$

$$m_{2} = 2$$

$$m_{2} = 1.5$$

$$m_{2} = 1.5$$

- (a)(10) If we sketch the fundamental mode power distribution for each waveguide, which waveguide has the largest y value for the peak power position? Explain.
- (b)(10) Among Type II, III, IV waveguides, which has the largest value for the fundamental mode effective index? Explain.
- (c)(10) Among Type II, III, IV waveguides, which has the largest value for the fundamental mode confinement factor? Explain.

Problem 2

(a)(10) From the b-V diagram provided separately, determine the wavelength range within which the fiber is a single-mode waveguide. Use n_1 (core reflective index)= 1.458, n_2 = 1.452, and a (core radius) = 3.5 μ m.

(b)(10) In a three-layer symmetric dielectric waveguide with n_1 (core reflective index)= 1.458, n_2 = 1.452, and d (core thickness) = 7 μ m, what is the wavelength range within which the waveguide has a single TE mode?

(c)(10) A singe mode fiber has loss of 0.2 dB/km at λ = 1.5 μ m. If 1 mW of 1.5 μ m light is introduced at the input, what is the output power at the end of 100km long fiber?

Problem 3

A symmetric three-layer waveguide is shown below. Consider only TE mode for this problem.

- (a) Determine how many modes the waveguide can support for λ=1.0μm.
- (b) Sketch the electric field intensity in the waveguide for each mode.
- (c) When λ is increased, the number of modes the waveguide can support may change. What is the largest wavelength for which the mode number remains the same as what was obtained in (a)?

